
FUNZIONE DESCRITTIVA

SISTEMI CON SEMPLICI NON LINEARITÀ

- Le caratteristiche dipendono dall'**ampiezza** dei segnali
- Lo studio è molto più complesso
- Difficile anche imporre **specifiche**



Non si applica
la sovrapposizione

Obiettivi minimi:

- Verificare la presenza di **oscillazioni**
- Calcolare i valori di **regime**

Ipotesi semplificative

- Una sola NL SISO nel loop
- La caratteristica è algebrica non differenziale

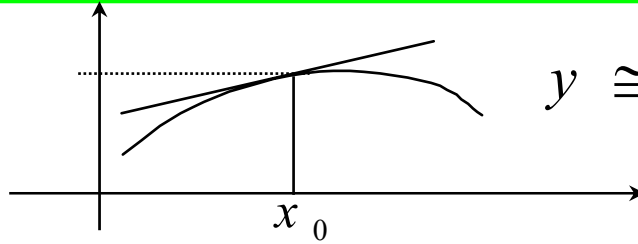


Non dipende da ω

(Rif. MARRO: Controlli Automatici)

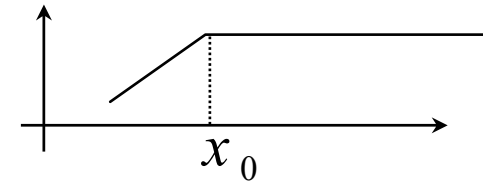
Taylor

- esatta per $\Delta x \rightarrow 0$
- adatta $\forall \Delta x(t)$
- Cade se Δx grande, ad es. oscillazioni
- Non utilizzabile se $\nexists f'(x_0)$



$$y \cong y_0 + f'(x_0)\Delta x$$

Si trascurano le derivate >1



Armonica

$$x \sin(\omega t) \rightarrow \boxed{L} \longrightarrow Kx \sin(\omega t + \varphi)$$

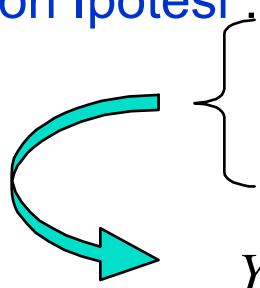
$$x \sin(\omega t) \rightarrow \boxed{NL} \longrightarrow \sum Y_i(x) \sin [i \omega t + \varphi_i(x)] \cong Y_0 + Y_1(x) \sin [\omega t + \varphi_1(x)]$$

Si trascurano le armoniche >1

- Non legata ad un punto di lavoro ma ad un tipo di ingresso
- Valida per ogni ampiezza

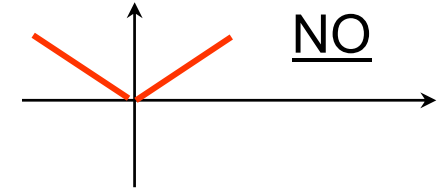
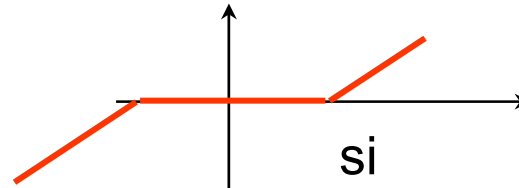
Sono entrambi sviluppi in serie di **funzioni ortogonali**

Ulteriori Ipotesi :



- Ingresso del sistema nullo
- Caratteristiche NL antisimmetriche

$$Y_0 \equiv 0$$



- la parte lineare è “**passa basso**” attenua le armoniche superiori



$$y(t) \cong Y_1(x) \sin [\omega t + \varphi_1(x)]$$

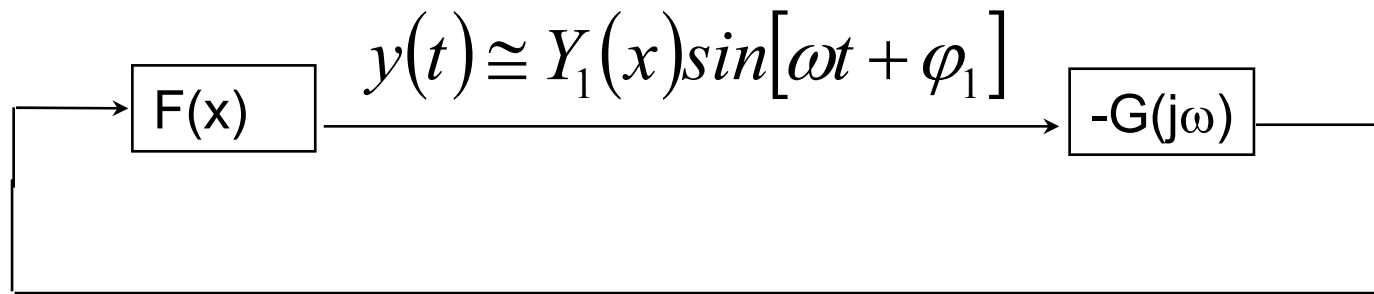
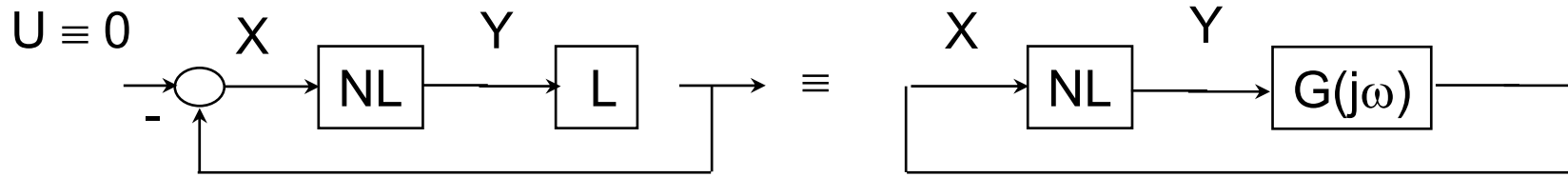
- Si definisce la “**FUNZIONE DESCRITTIVA**”

$$F(x) = \frac{1}{x} \cdot Y_1(x) \cdot e^{j\varphi_1(x)}$$

Complessa!

- Si approssimano le **oscillazioni** (**cicli limite**) con andamenti sinusoidali
- F(x) quasi una funzione di trasferimento, un guadagno variabile

METODO DELLA FUNZIONE DESCRITTIVA



$$x \sin \omega t \xrightarrow{F(x)} Y_1(x) \sin[\omega t + \varphi_1] \xrightarrow{-G(j\omega)} x \sin \omega t$$

Condizioni
per un ciclo
limite $\bar{x}, \bar{\omega}$

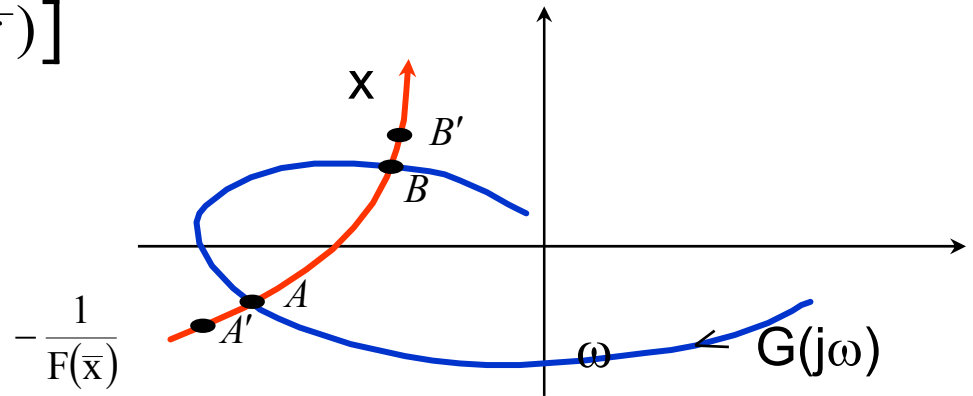
$$\begin{cases} |G(j\bar{\omega})| \cdot Y_1(\bar{x}) = \bar{x} \\ \angle G(j\bar{\omega}) + \varphi_1(\bar{x}) = 180^\circ \end{cases} \longrightarrow |G| = \frac{1}{|F|}$$

Interpretazione Grafica

$$\arg[G(j\bar{\omega})] = 180^\circ - \arg[F(\bar{x})]$$

$$|G(j\bar{\omega})| = \frac{1}{|F(\bar{x})|}$$

$$\boxed{-\frac{1}{F(\bar{x})} = G(j\bar{\omega})}$$

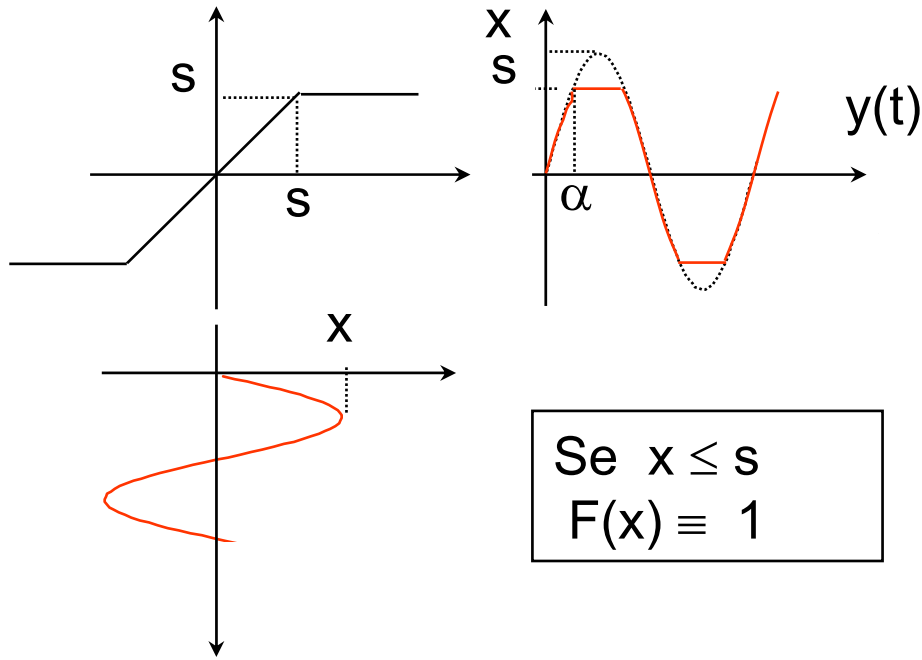


Quando c'è intersezione c'è un ciclo limite

A : instabile se diminuisce (A') occorrerebbe $|G|$ maggiore

B : stabile se aumenta (B') con $|G| = \text{cost}$,
 può ridiminuire e tornare a B

ESEMPIO DI CALCOLO (SATURAZIONE)



Se $x \leq s$
 $F(x) \equiv 1$

Occorre calcolare la
1^a armonica di $y(t)$

$$F(x) = \frac{1}{x} [b_1(x) + ja_1(x)]$$

$$b_1 = \frac{1}{\pi} \int_{-\pi}^{\pi} y(t) \sin(\omega t) d\omega t$$

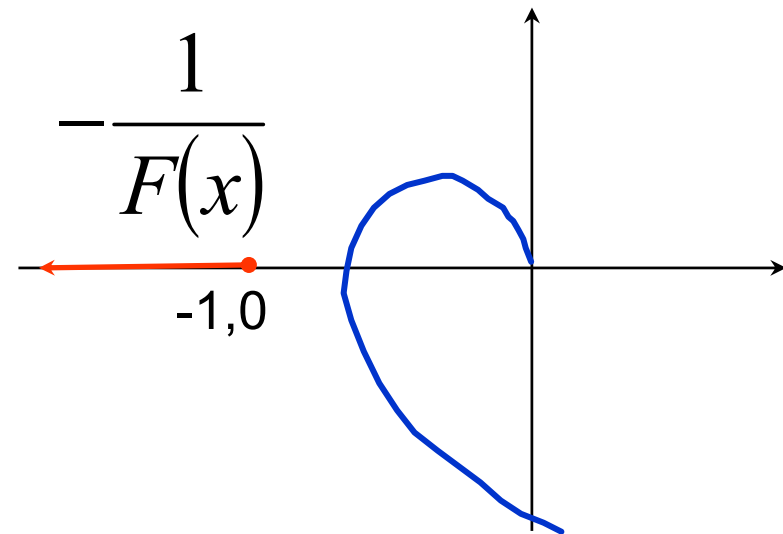
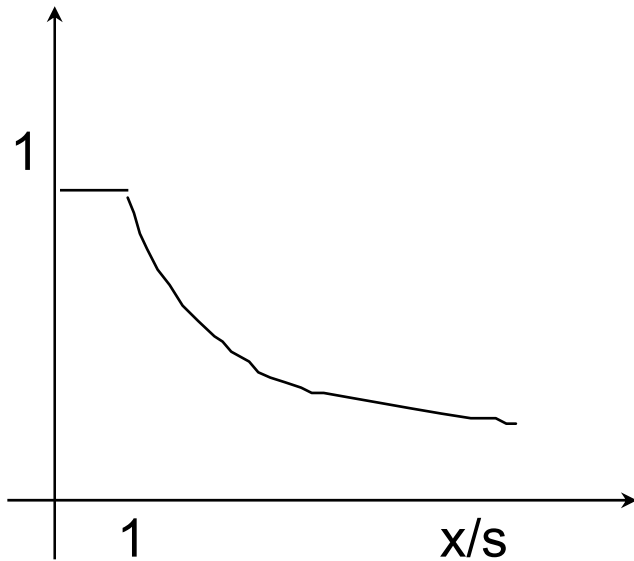
$$a_1 = \frac{1}{\pi} \int_{-\pi}^{\pi} y(t) \cos(\omega t) d\omega t$$

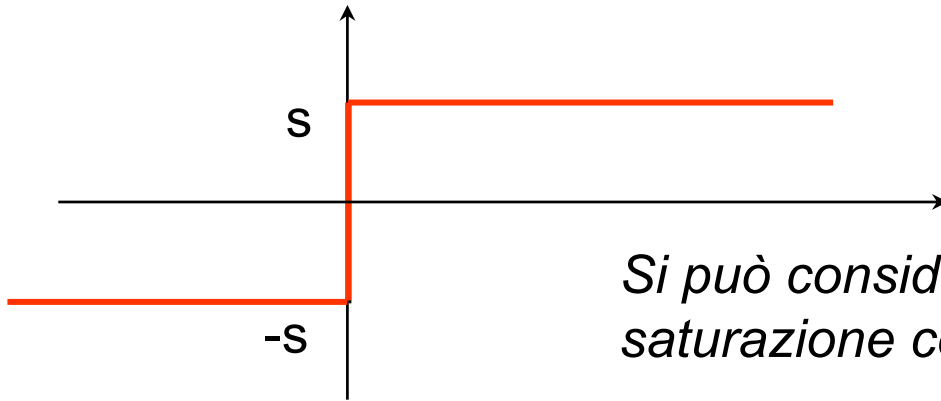
Per la simmetria $a_1 \equiv 0$ $F(x)$ solo Reale

$$b_1 = \frac{4}{\pi} \int_0^{\frac{\pi}{2}} \dots \dots = \frac{4}{\pi} \left[\int_0^{\alpha} x \cdot \sin^2 \omega t \cdot d\omega t + \int_{\alpha}^{\frac{\pi}{2}} s \cdot \sin \omega t \cdot d\omega t \right] \quad \alpha = \sin^{-1} \left(\frac{s}{x} \right)$$

ESEMPIO DI CALCOLO (SATURAZIONE)

$$F(x) = \begin{cases} 1 & x \leq s \\ \frac{2}{\pi} \left[\sin^{-1} \left(\frac{s}{x} \right) + \frac{s}{x} \sqrt{1 - \left(\frac{s}{x} \right)^2} \right] & x > s \end{cases}$$

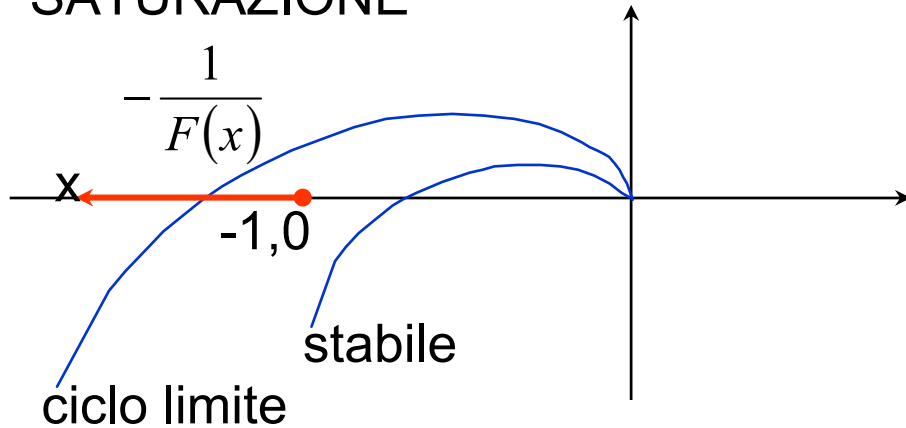




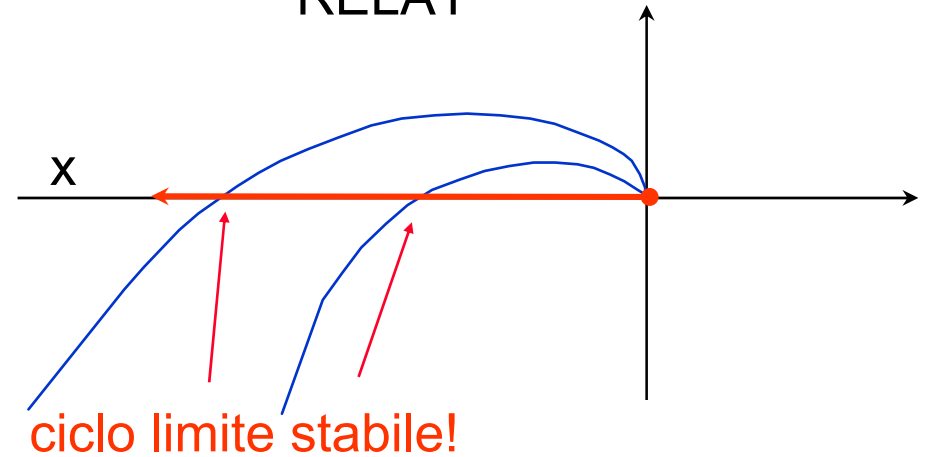
$$F(x) = \frac{4s}{\pi x}$$

Si può considerare come una saturazione con guadagno infinito

SATURAZIONE



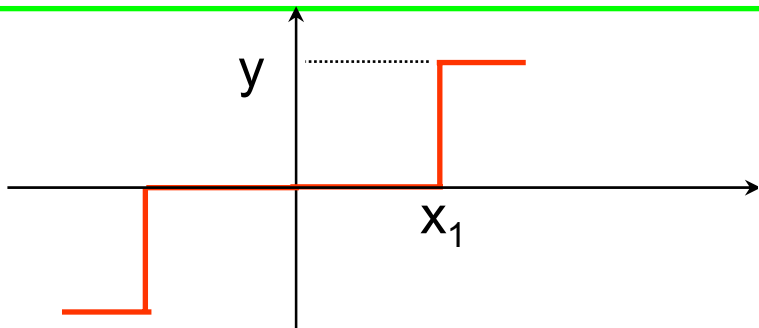
RELAY



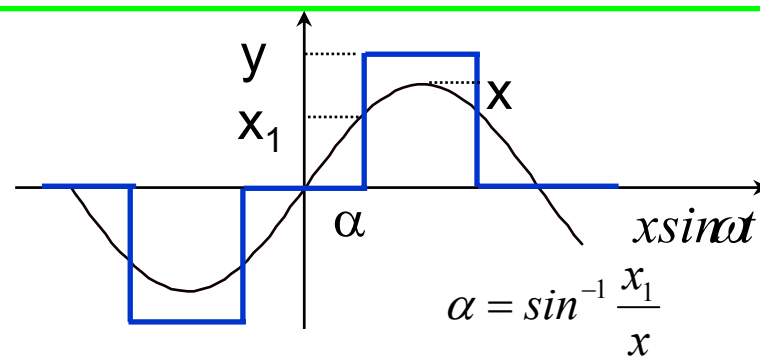
Si noti che per piccoli sfasamenti
o $|G| \rightarrow 0$

$$\begin{cases} \omega \rightarrow \infty \\ \bar{x} \rightarrow 0 \end{cases}$$

RELAY CON SOGLIA

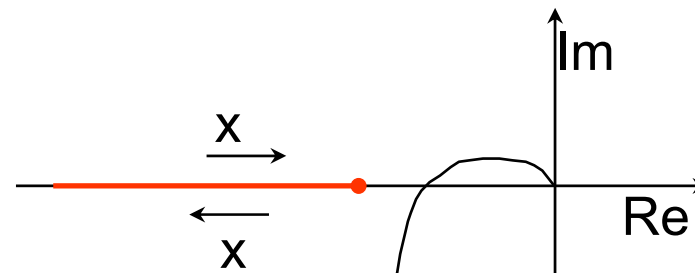
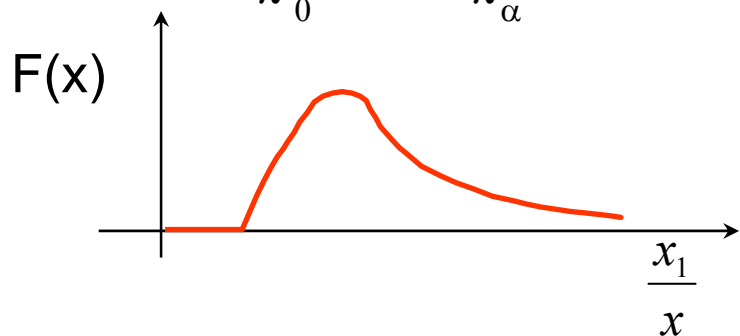


Simmetria $a_1 = 0$

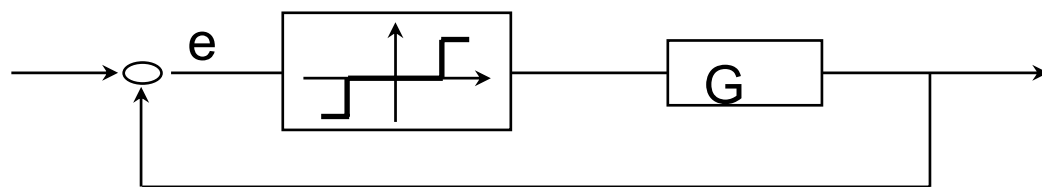


$$b_1 = \frac{4}{\pi} \int_0^{\frac{\pi}{2}} \dots = \frac{4}{\pi} \int_0^{\frac{\pi}{2}} Y_1 \cdot \sin \omega t \cdot d\omega t =$$

$$\begin{cases} 0 & x \leq x_1 \\ \frac{4Y_1}{\pi} \sqrt{1 - \left(\frac{x_1}{x}\right)^2} & x > x_1 \end{cases}$$

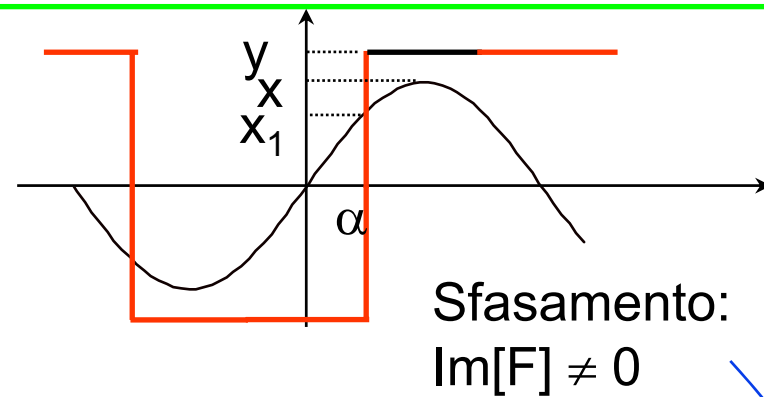
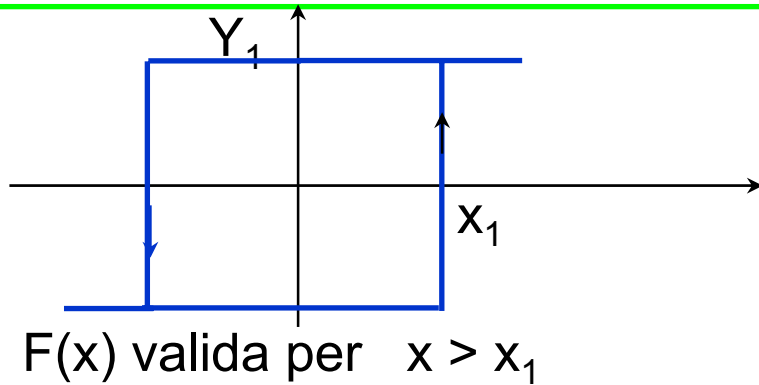


Due intersez. : un ciclo stabile
uno instabile



$-x_1 \leq e \leq x_1$
ciclo aperto!

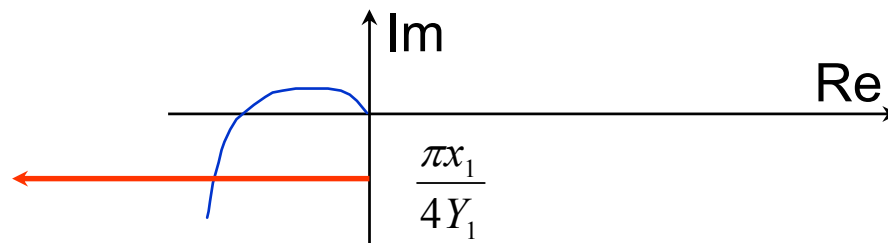
RELAY CON ISTERESI

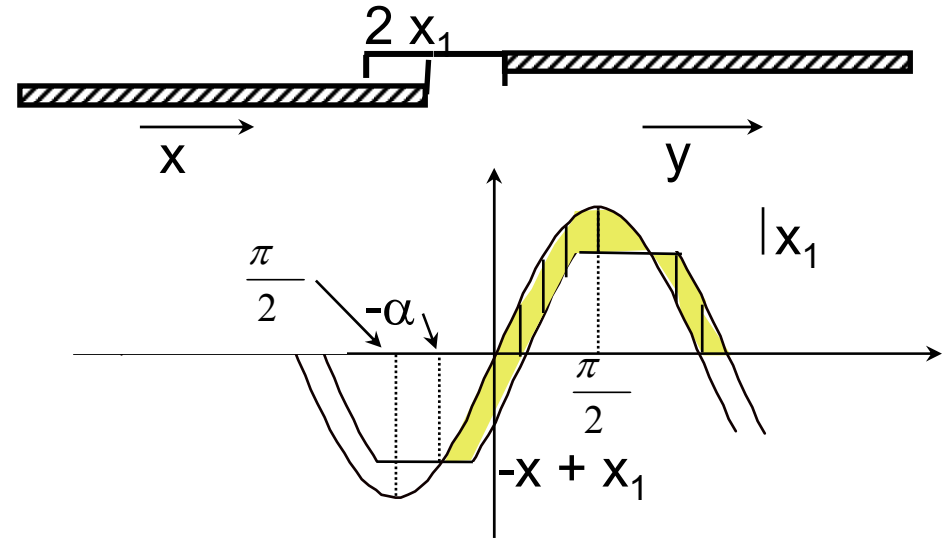
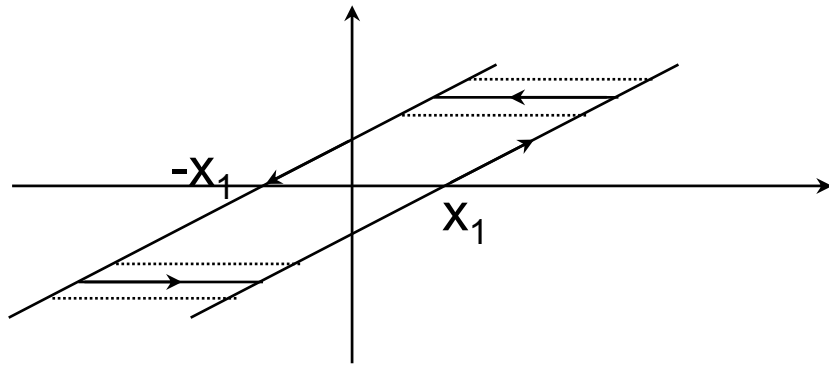


$$a_1 = -\frac{4Y_1}{\pi} \cdot \frac{x_1}{x}, \quad b_1 = \frac{4Y_1}{\pi} \cdot \sqrt{1 - \left(\frac{x_1}{x}\right)^2}$$

$$F(x) = \frac{1}{x}(b_1 + ja_1) = \frac{4Y_1}{\pi x} \left(\sqrt{1 - k^2} - jk \right)$$

$$-\frac{1}{F(x)} = \frac{\pi x}{4Y_1} \left(\sqrt{1 - k^2} + jk \right) = -\frac{\pi x}{4Y_1} \left[\sqrt{1 - \left(\frac{x_1}{x}\right)^2} + j \frac{x_1}{x} \right]$$



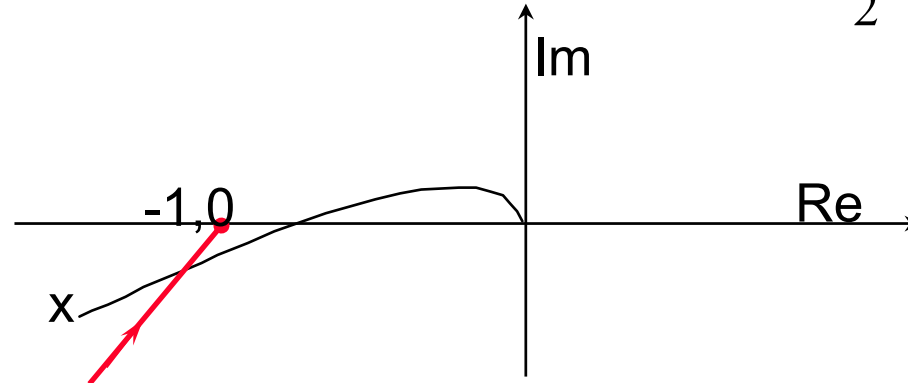


$$y(t) = -x + x_1$$

$$-\frac{\pi}{2} \leq \omega t \leq -\alpha$$

$$y(t) = x \cdot \sin \omega t - x_1$$

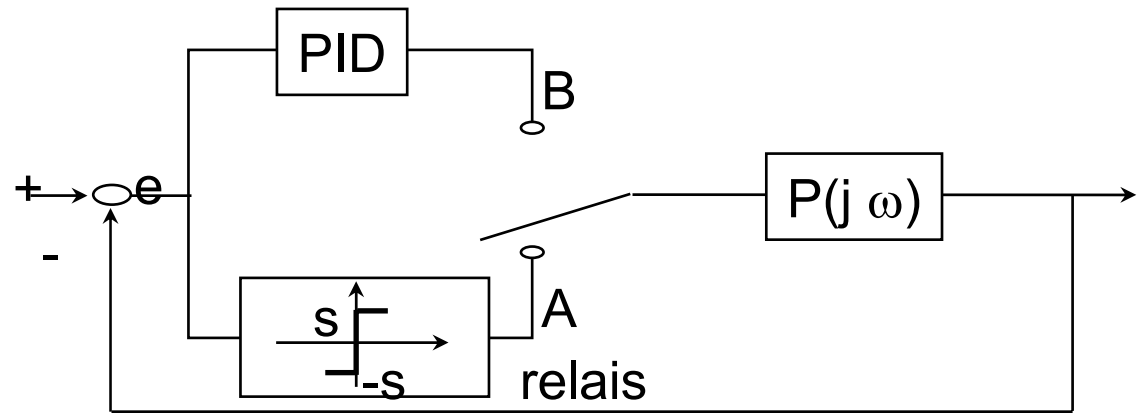
$$-\alpha \leq \omega t \leq \frac{\pi}{2}$$



UN METODO PER L'AUTOTUNING DEI REGOLATORI

A: il sistema oscilla
si misurano e e ω per
determinare ω_L e k_L

B: Normale
Funzionamento

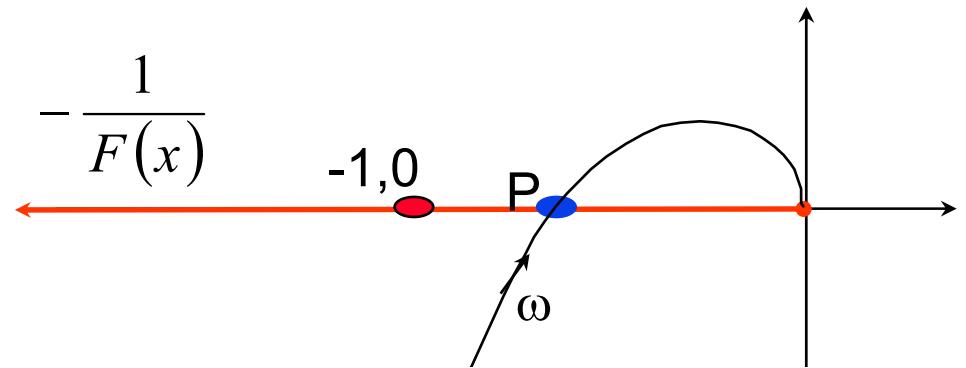


$$F(x) = \frac{4S}{\pi x}$$

$$x \equiv |e|$$

$$\frac{1}{m_g} = \frac{\pi x}{4S}, \quad \omega_L = \bar{\omega}$$

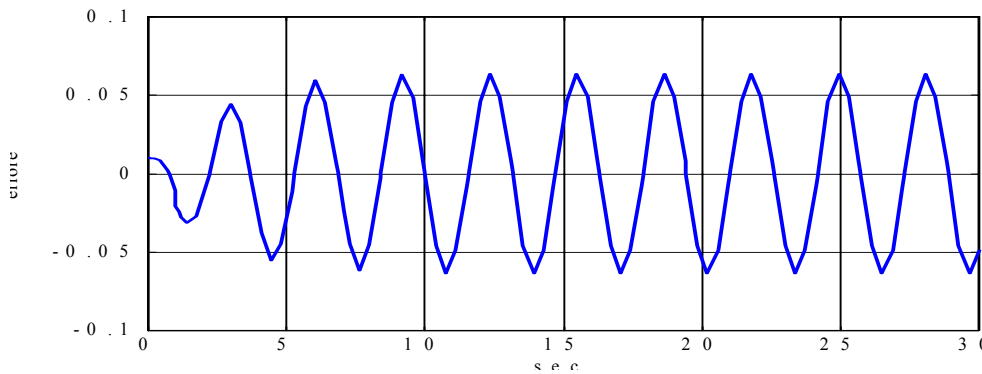
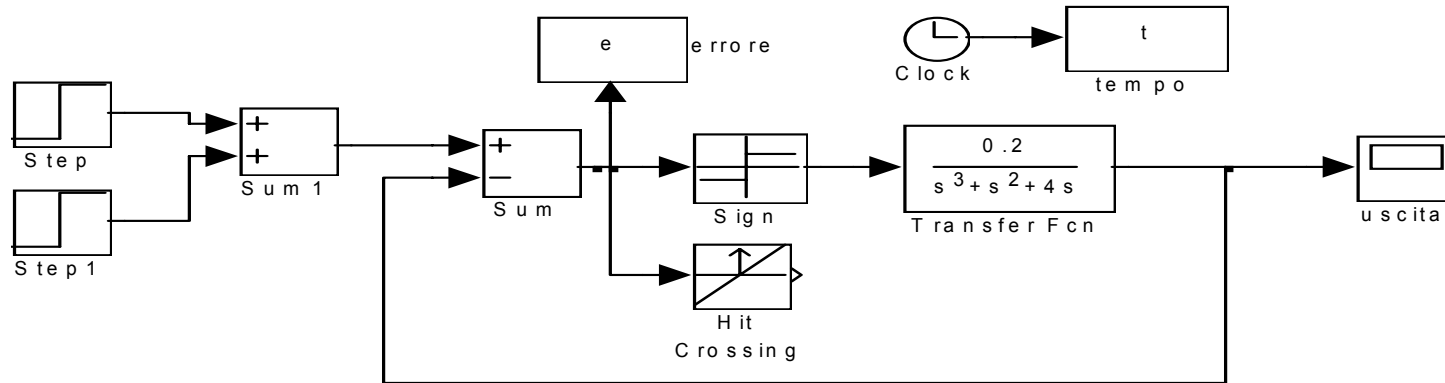
m_g = margine di guadagno



Si individua
la posizione di P
dalle misure

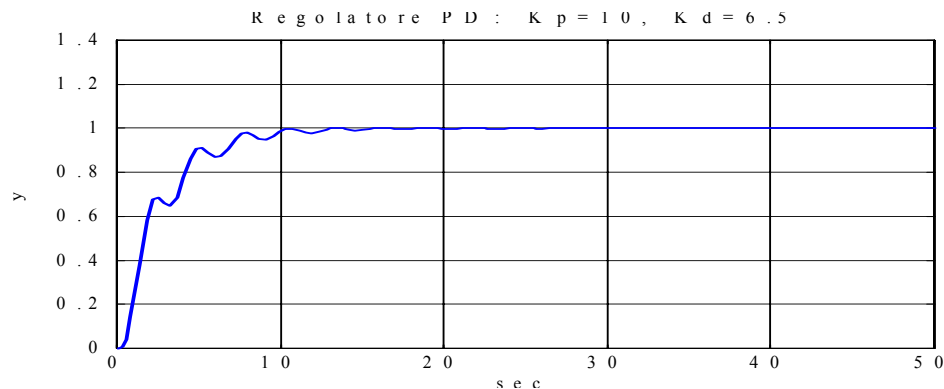
In base a questi valori si calcolano k_p , k_i , k_d

Poi si commuta sul PID



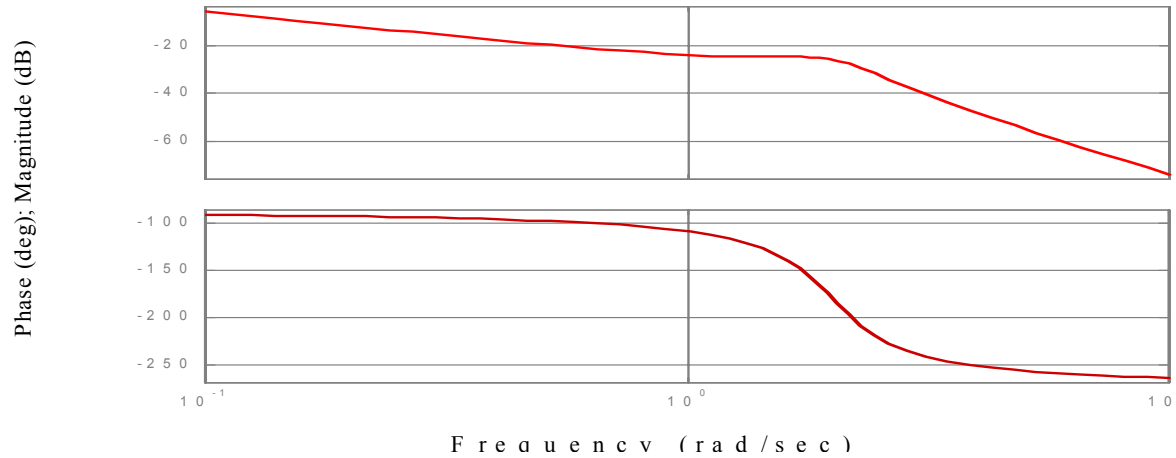
Con il relè:
 $m_g = 20$
 $\omega_L = 2.01 \text{ rad/sec}$

Usando un
 regolatore
 Proporzionale
 Derivativo



Dai diagrammi di Bode e Nyquist:

B o d e D i a g r a m s



N y q u i s t D i a g r a m s

