
RISPOSTA ARMONICA

(VEDI MARRO PAR. 3.1 A 3.2)

(VEDI VITELLI-PETTERNELLA PAR.VII.2, VII.2.1)

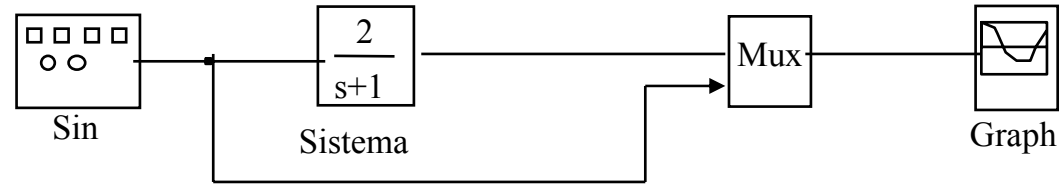
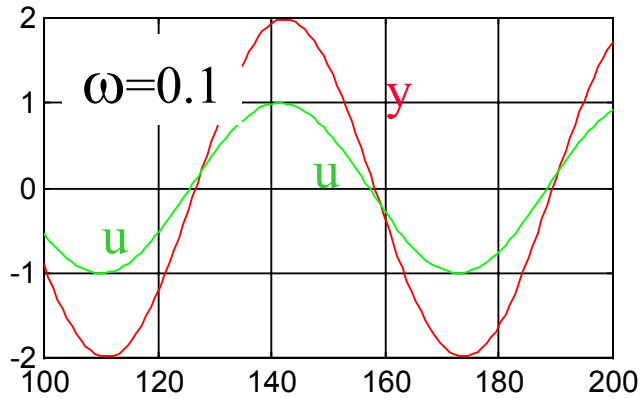
CHE COSA E'

COME SI CALCOLA

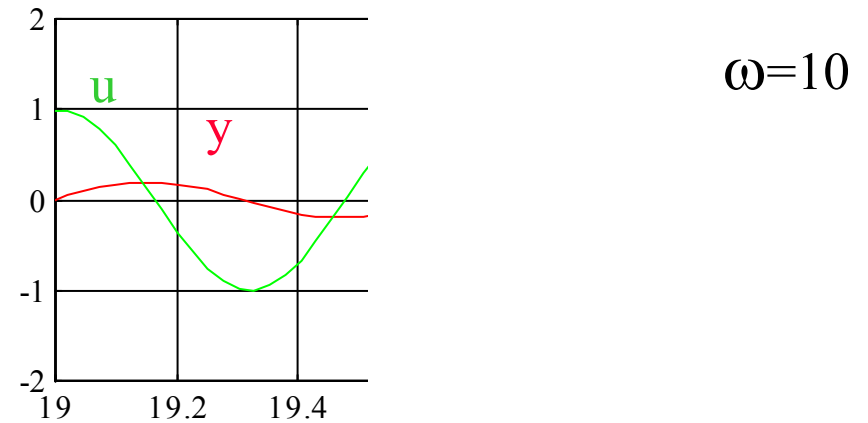
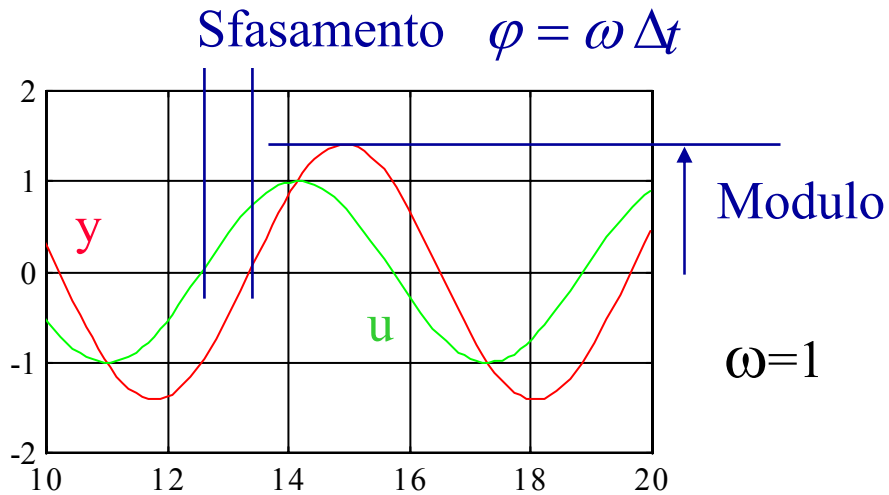
(COME SI MISURA)

CRITERI DI STABILITA'

CHE COSA È (VEDI BODEUNPOLO_N.VI RELIZZATO CON LABVIEW)

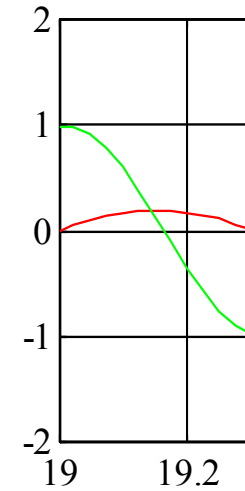
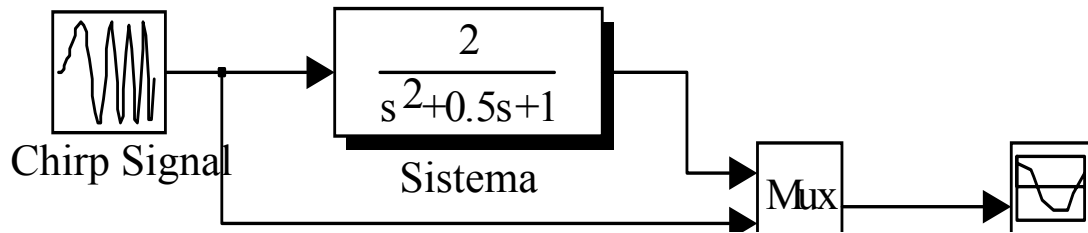


Risposta Armonica:
 $M(\omega)$ e $\varphi(\omega)$ di $Y(j\omega)/U(j\omega)$

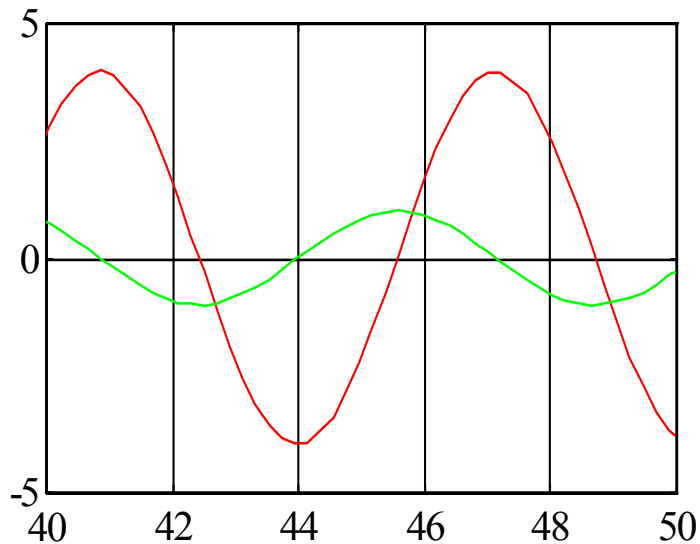


$\omega=10$

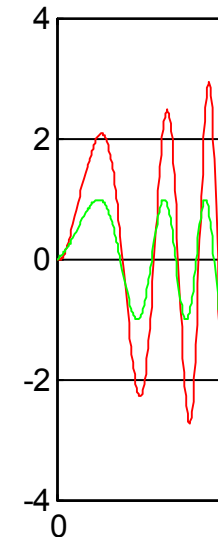
Alcune frequenze sono enfatizzate



$\omega=0.1$



$\omega=0.06-2.4$



- $G(s)$: asintoticamente stabile, $\text{Re}[p_i] < 0 \quad \forall p_i$

$$u(t) \begin{cases} \sin \omega t & t > 0 \\ 0 & t \leq 0 \end{cases} \quad U(s) = \frac{\omega}{s^2 + \omega^2}$$

$$Y(s) = G(s) \cdot U(s) = G(s) \cdot \frac{\omega}{s^2 + \omega^2} = G(s) \cdot \frac{\omega}{(s + j\omega) \cdot (s - j\omega)} = Y_t(s) + \underbrace{\frac{R}{s - j\omega} + \frac{R^*}{s + j\omega}}_{\text{permanente}}$$

↑
Fattorizzazione

$$\text{con } R = \lim_{s \rightarrow j\omega} (s - j\omega) \cdot Y(s) = \lim_{s \rightarrow j\omega} G(s) \frac{\omega}{s + j\omega} = \frac{1}{2j} G(j\omega)$$

$$y(t) = y_t(t) + \frac{1}{2j} \left[G(j\omega) \cdot e^{j\omega t} - G^*(j\omega) \cdot e^{-j\omega t} \right] =$$

$$= \cancel{y_t(t)} + \underbrace{|G(j\omega)| \cdot \sin(\omega t + \angle G(j\omega))}_{\text{permanente}}$$

$$G(s)_{s=j\omega} = G(j\omega)$$

risposta armonica

Transitorio $\rightarrow 0$

SCOMPOSIZIONE IN TERMINI SEMPLICI

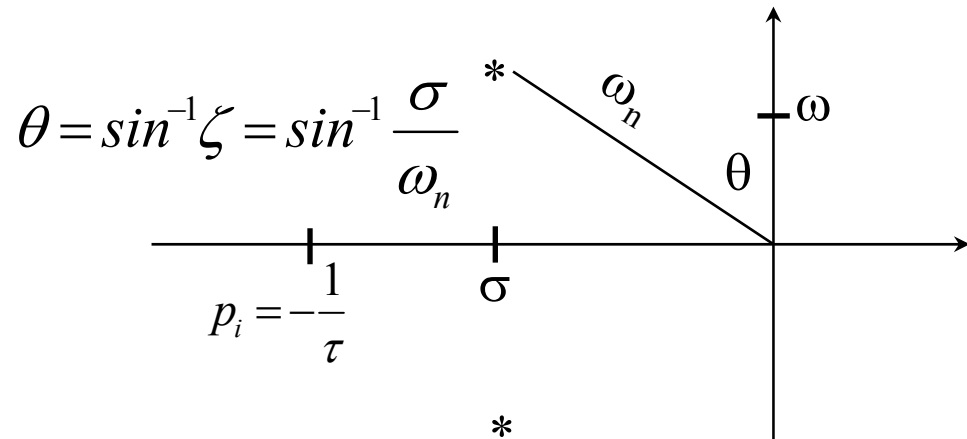
Per $G(s)$ razionale: $G(j\Omega) = \sum$ tre tipi di termini (e loro reciproci) quando

$$G(s) = \frac{\sum b_j s^j}{\sum a_i s^i} = \frac{N(s)}{D(s)}$$

Per ogni polinomio le **radici** possono essere:

• $p_i = 0$	→	s	s
• p_i : reale	→	$(s-p_i)$	$1+\tau s$
• p_i, p_j coppia c.c.	→	$[s^2-2\sigma s+(\sigma^2+\omega^2)]$	$1+\frac{2\zeta}{\omega_n} s + \frac{s^2}{\omega_n^2}$
Termini della fattorizzazione			Notazione usuale

τ : costante di tempo
 ω_n : pulsazione di risonanza
 ζ : smorzamento, $0 \div 1$



SCOMPOSIZIONE IN TERMINI SEMPLICI - 2

Comportamento asintotico $G(j\omega)$:

$$G(s) = K \cdot \frac{\prod (1 + \tau_i s) \prod \left(1 + \frac{2\zeta_i s}{\omega_{ni}} + \frac{s^2}{\omega_{ni}^2} \right)}{s^h \prod (1 + \tau_j s) \prod \left(1 + \frac{2\zeta_j s}{\omega_{nj}} + \frac{s^2}{\omega_{nj}^2} \right)} = \frac{b_m s^m + \dots + b_0}{a_n s^n + \dots + a_0}$$

$j\omega \rightarrow 0 \cong t \rightarrow \infty$

$$G(j\omega) \rightarrow \frac{K}{(j\omega)^h}$$

$$\text{se } \begin{cases} h = 0 & G(j\omega) = k = \frac{b_0}{a_0} \\ h > 0 & |G(j\omega)| \rightarrow \infty \\ & \angle G(j\omega) \rightarrow -h \cdot 90^\circ \end{cases}$$

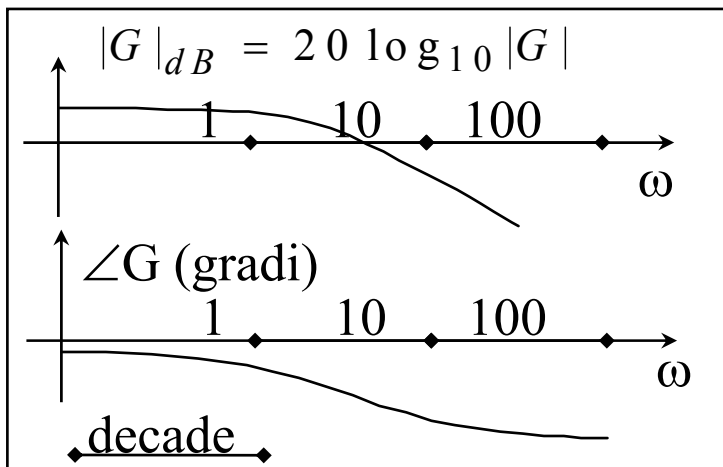
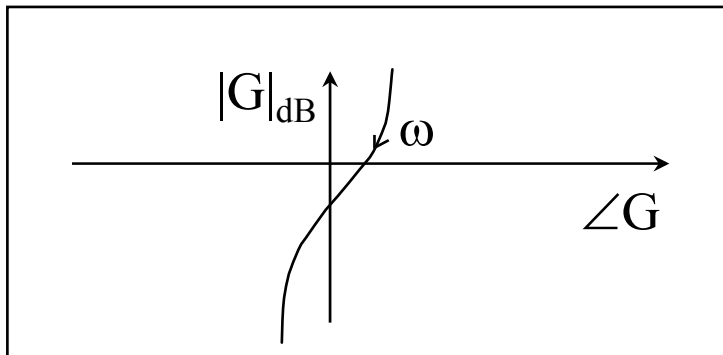
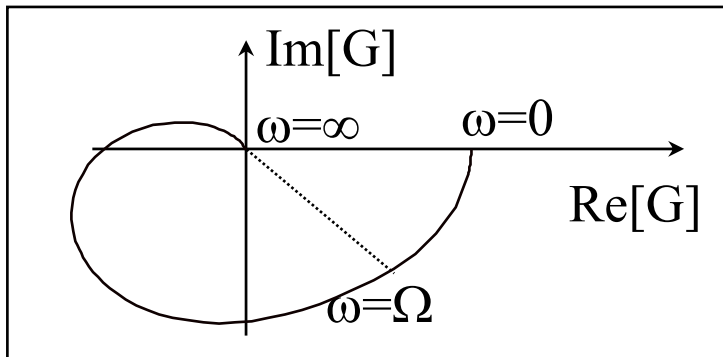
$j\omega \rightarrow \infty \cong t \rightarrow 0$

$$G(j\omega) \rightarrow \frac{b_m}{a_n} (j\omega)^{m-n}$$

$$\text{se } \begin{cases} m < n & \frac{b_m}{a_n} \cdot \frac{1}{(j\omega)^{n-m}} \quad |\cdot| \rightarrow 0 \quad \angle \cdot \rightarrow -(n-m) \cdot 90^\circ \\ m = n^* & |\cdot| \rightarrow \frac{b_m}{a_n} \quad \angle \cdot \rightarrow 0^\circ \\ n > m & \text{non può accadere} \end{cases}$$

* natura “*passa-basso*” dei sistemi fisici \Leftrightarrow CAUSALITA’

RAPPRESENTAZIONI DI $G(j\omega)$ (VEDI ES. REALIZZATI IN SCILAB)



(vedi NumDenPoli_n.vi realizzato in LabView)

Polare o Re-Im (parametro= ω) : NYQUIST

(vedi Marro par. 3.5, vedi Vitelli-Petternella par. VIII.3)

- Poco usato in pratica, utile in certe dimostrazioni.

Modulo-fase (parametro= ω) : NICHOLS

(vedi Marro par. 3.6, vedi Vitelli-Petternella par. VIII.2)

- Un tempo usata la carta di Nichols nella progettazione, oggi non più.

Modulo e fase separati : BODE

(vedi Marro par. 3.3, vedi Vitelli-Petternella par. VII.3)

- Ancora estremamente diffuso
- Usato nella strumentazione, come output dei calcolatori
- Usato nella progettazione manuale ed assistita

•Bell : $B = \log_{10} \frac{W_2}{W_1}$

•Decibel : $\text{dB} = 10 \log_{10} \frac{A_2}{A_1}$

Poiché $W \propto V^2, I^2 \dots$

Es.: $W=RI^2$ W : potenza quando si usano le ampiezze :

Decibel: $\text{dB} = 20 \log_{10} \frac{A_2}{A_1}$

Vantaggi:

- campo di valori maggiore a parità d'ingombro
- errore di rappresentazione costante in percentuale
- alcuni andamenti si semplificano

Alcuni valori

$0.1 \text{ dB} = -20$

$2 \text{ dB} \cong 6$

$10 \text{ dB} = 20$

$20 \text{ dB} \cong 26$

$1 \text{ dB} = 0$

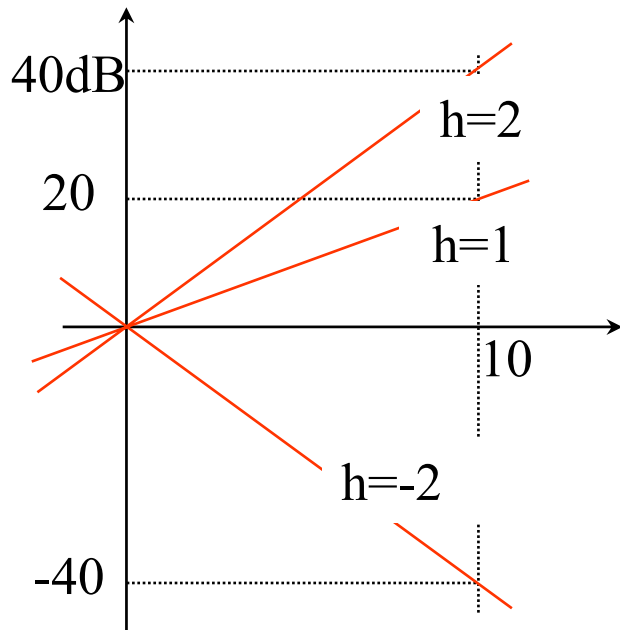
$100 \text{ dB} = 40$

$$\left| \frac{1}{G(j\omega)} \right|_{\text{dB}} = - \left| G(j\omega) \right|_{\text{dB}}$$

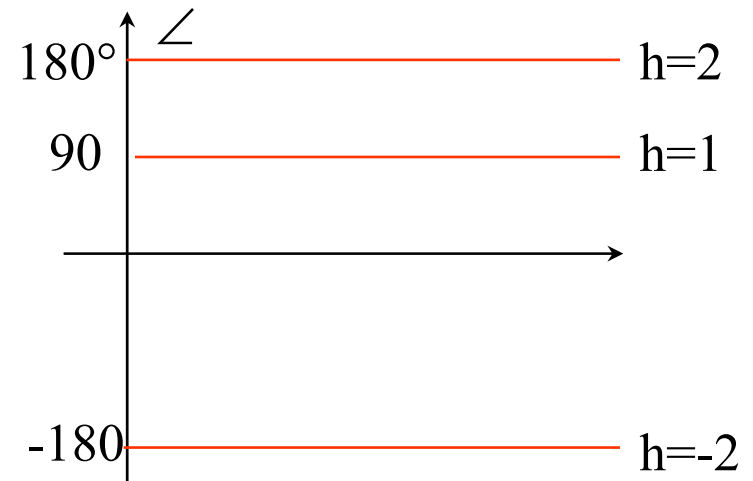
$j\omega^h$

λ	-1	0	1	2
w	0.1	1	10	100

Modulo = $20 h \log \omega = 20 h \lambda$



Fase = $90^\circ h$

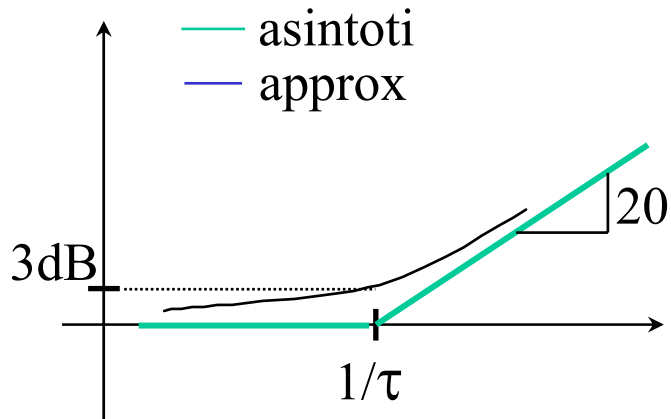


TERMINE BINOMIO $(1 + j\omega\tau)$

(vedi BodeUnPolo_n.vi realizzato in LabView)

$$| \cdot | = 20 \log \sqrt{1 + \omega^2 \tau^2} = 10 \log(1 + \omega^2 \tau^2)$$

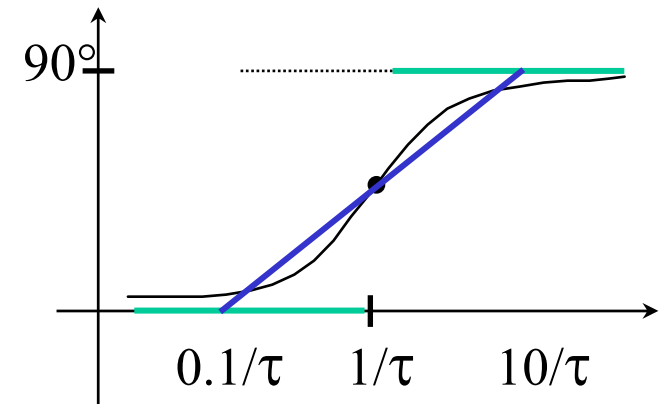
$$\begin{cases} \omega \ll \frac{1}{\tau} & 10 \log 1 = 0 \\ \omega \gg \frac{1}{\tau} & 10 \log \omega^2 \tau^2 = 20 \log \tau + 20 \lambda \end{cases}$$



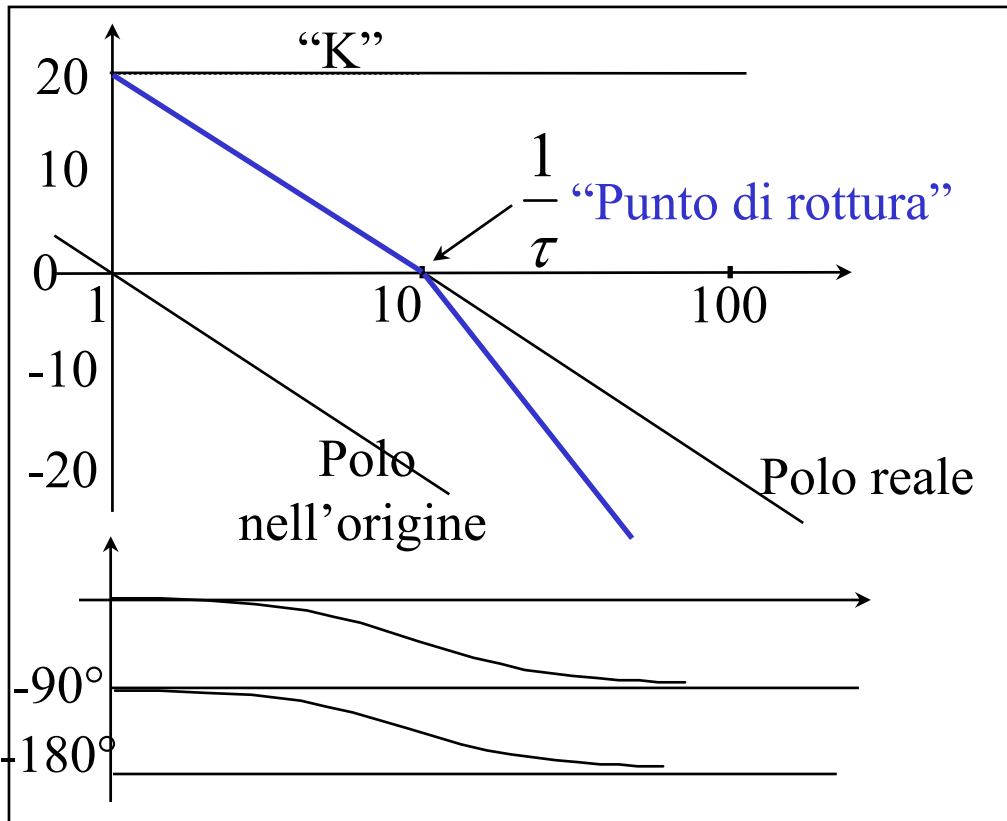
$$|1/G(j\omega)|_{\text{dB}} = -|G(j\omega)|_{\text{dB}}$$

$$\angle(1 + j\omega\tau) = \tan^{-1}\left(\frac{\omega\tau}{1}\right)$$

$$\begin{cases} \omega \ll \frac{1}{\tau} & \text{tg}^{-1}(0) = 0 \\ \omega \gg \frac{1}{\tau} & \text{tg}^{-1}(\infty) = 90^\circ \\ \omega = \frac{1}{\tau} & \text{tg}^{-1}(1) = 45^\circ \end{cases}$$



$$\angle 1/G(j\omega) = -\angle G(j\omega)$$



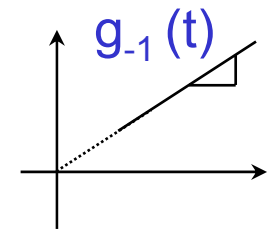
non è K! fattore di guadagno K

$$\bullet G(s) = \frac{100}{s(s+10)} = \frac{10}{s(1+0.1s)}$$

polo nell’origine polo reale

• **Significato di K**

$$\lim_{s \rightarrow 0} s \cdot \frac{1}{s} \cdot \frac{100}{s(s+10)} = \infty$$



pendenza .. $sG(s)$

$$\lim_{s \rightarrow 0} s \cdot \frac{1}{s} \cdot s \cdot \frac{100}{s(s+10)} = 10$$

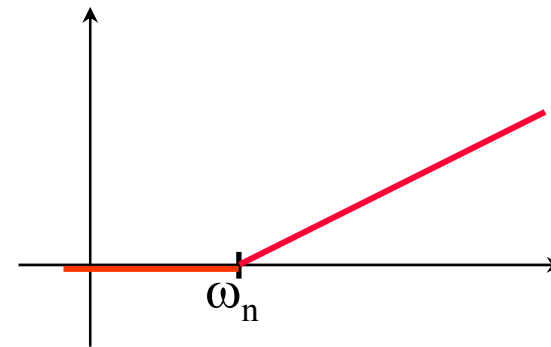
$$W_3(s) = 1 + \frac{2\zeta}{\omega_n} s + \frac{s^2}{\omega_n^2}$$

• Rappresenta “*modi pseudoperiodici*”

- **RISONANZE** (Denominatore) e
- **ANTIRISONANZE** (Numeratore)

$$W_3(s) \Big|_{s=j\omega} = \begin{cases} \omega \rightarrow 0 & , \quad 1 \\ \omega \rightarrow \infty & , \quad -\frac{\omega^2}{\omega_n^2} \end{cases}$$

$$\|dB\| = \begin{cases} 0 \\ -40 \log \omega_n + 40 \lambda \\ (\lambda = \log \omega) \end{cases}$$



Per $\omega = \omega_n$

$$W_3 = 1 + 2j\zeta \frac{\omega_n}{\omega_n} - \frac{\omega_n^2}{\omega_n^2} = 2j\zeta \quad \left\{ \begin{array}{l} |W_3(j\omega_n)| = 2\zeta \quad (\zeta = 0 \div 1) \\ \angle = +90^\circ \end{array} \right.$$

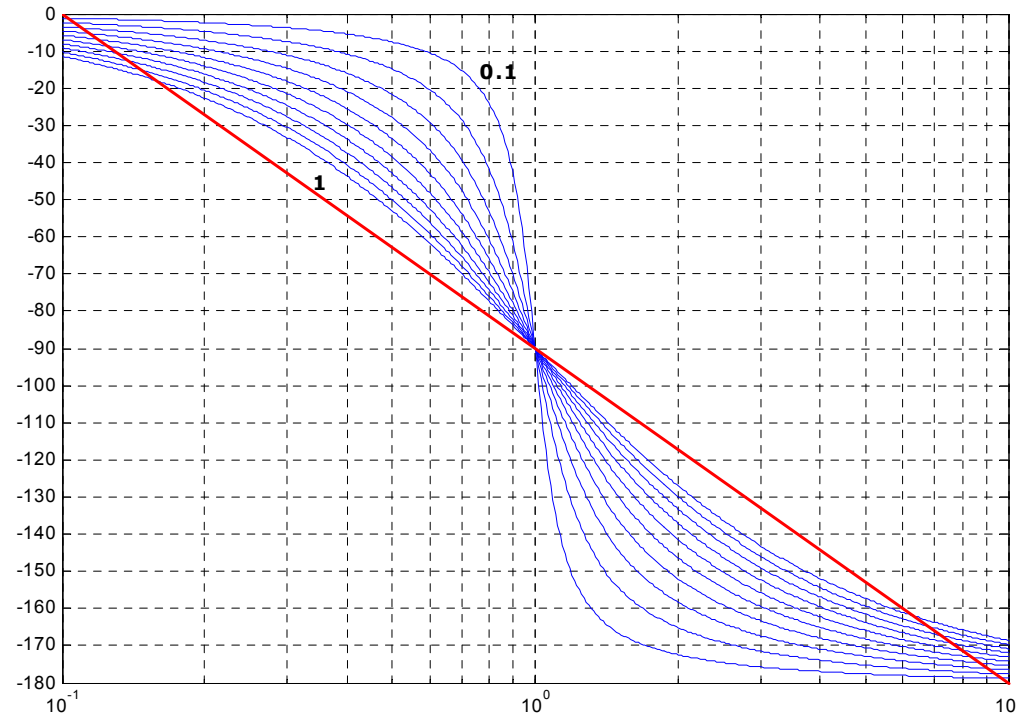
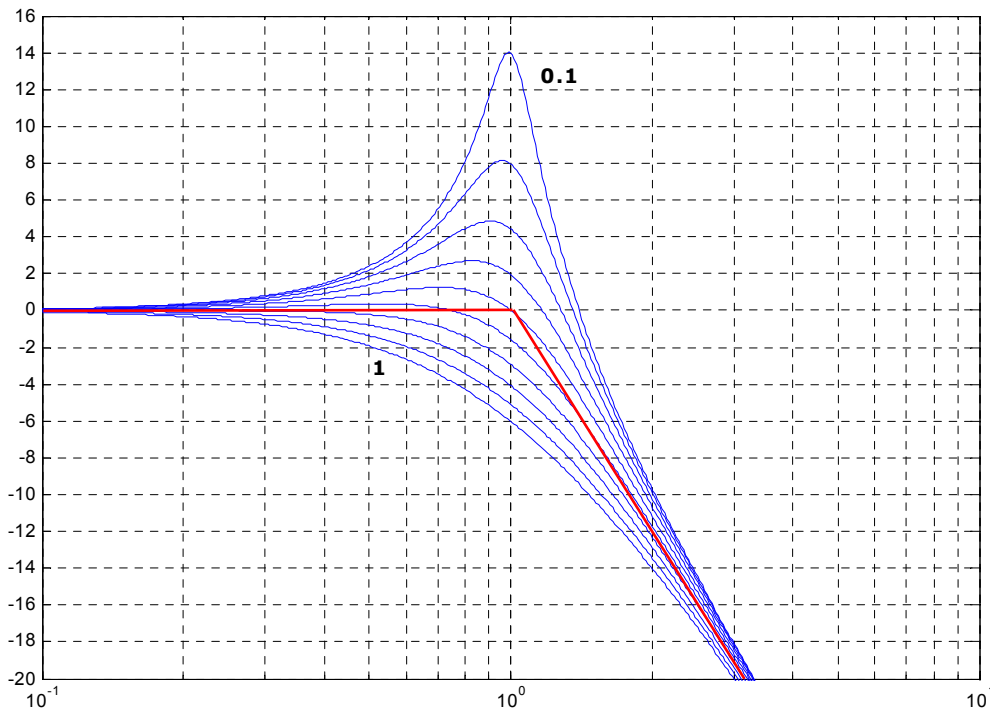
RISP. ARMONICA TERMINE TRINOMIO

(vedi BodeDuePoli_n.vi realizzato in LabView)

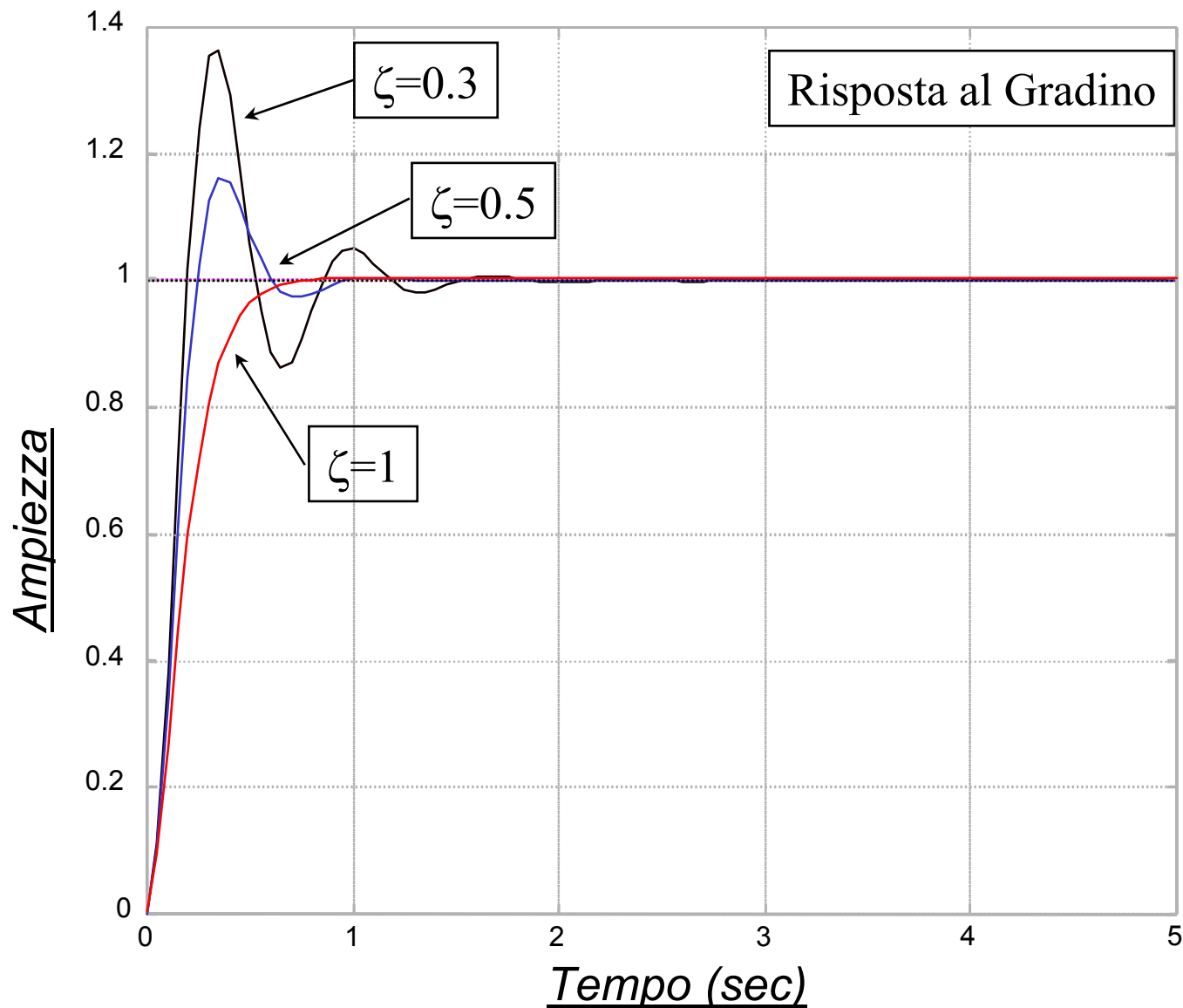
$$\frac{1}{W_3}$$

$$\omega_n = 1$$

$$\frac{1}{W_3}$$



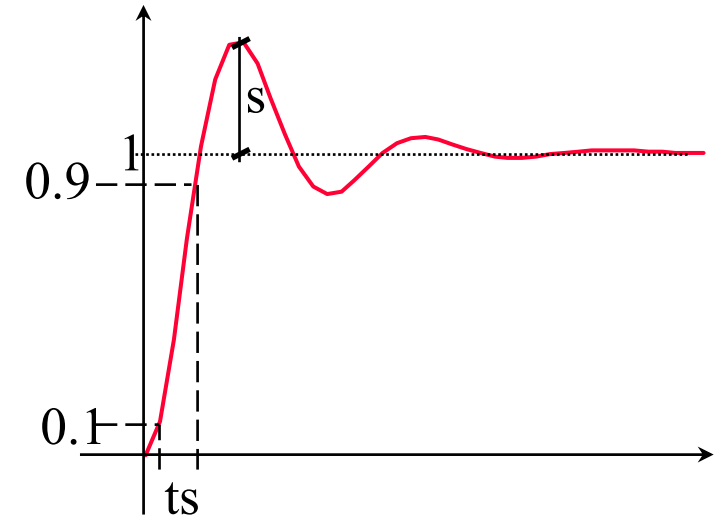
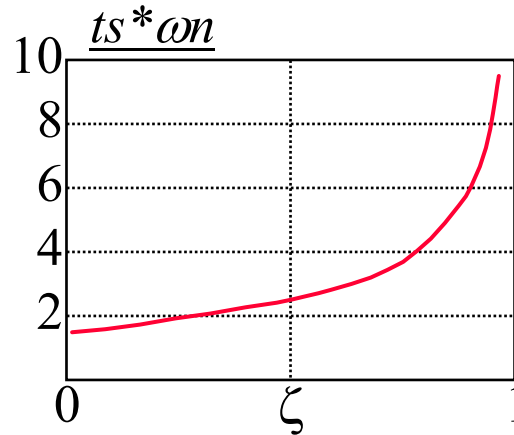
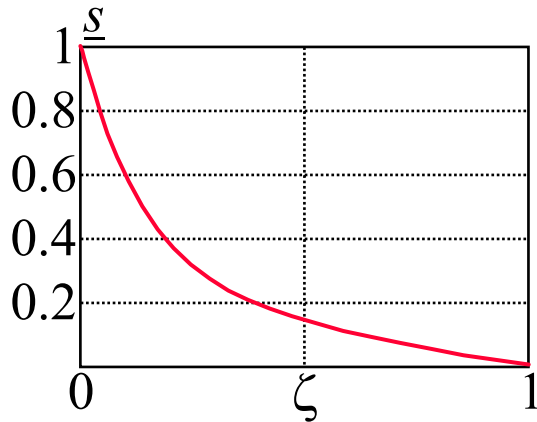
RISPOSTA AL GRADINO DEL TERMINE TRINOMIO



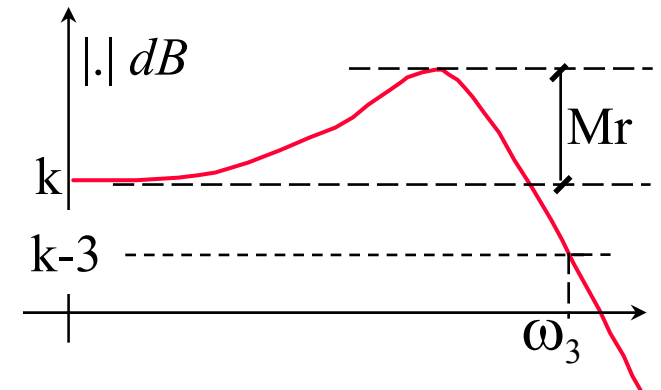
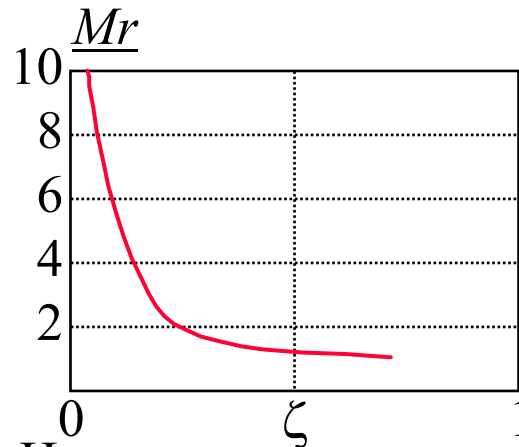
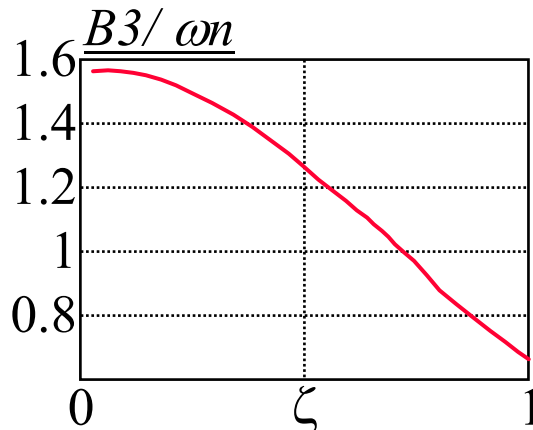
$$L^{-1} \left[\frac{1}{s} \cdot \frac{1}{1 + \frac{2\zeta}{\omega_n} s + \frac{s^2}{\omega_n^2}} \right]$$

PARAMETRI DEL T. TRINOMIO IN FUNZIONE DI ζ

Tempo



Frequenza



Attenzione : $B_3 = \omega_3 / 2\pi$ in Hz

ω_n in rad/sec

1^a massa: $M\ddot{x}_1 = f(t) - K(x_1 - x_2)$

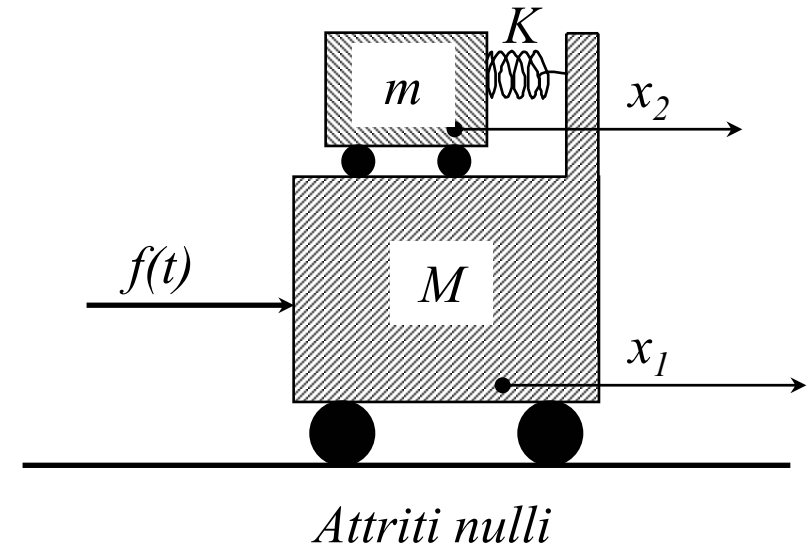
2^a massa: $m\ddot{x}_2 = K(x_1 - x_2)$

Trasformando :

$$\begin{cases} (Ms^2 + K) \cdot X_1(s) = F(s) + K \cdot X_2(s) \\ (ms^2 + K) \cdot X_2(s) = K \cdot X_1(s) \end{cases}$$

$$X_1(s) \left[(Ms^2 + K) - \frac{K^2}{ms^2 + K} \right] = F(s)$$

$$\frac{X_1(s)}{F(s)} = \frac{ms^2 + K}{(Ms^2 + K)(ms^2 + K) - K^2} = \frac{ms^2 + K}{[mMs^2 + K(m + M)] \cdot s^2}$$



N.B.

ω di antirisonanza è il punto in cui si annulla il numeratore

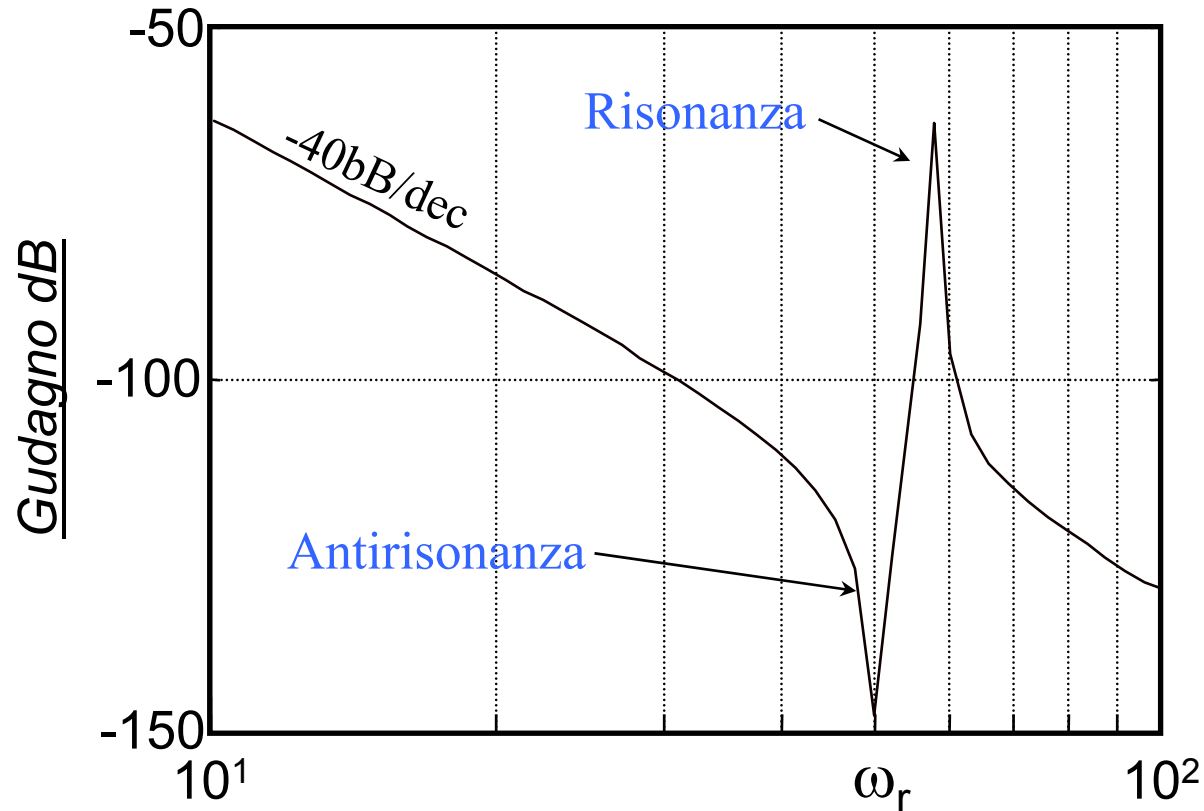
ω di risonanza è il punto in cui si annulla il denominatore

ESEMPIO (CONTINUA)

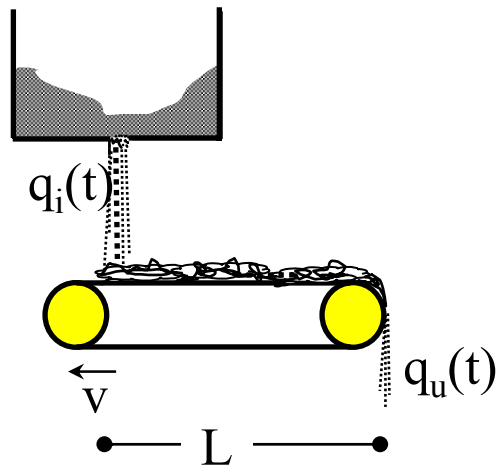
$$Ms^2 + K = 0 \quad \omega_r = \sqrt{\frac{K}{m}}$$

per

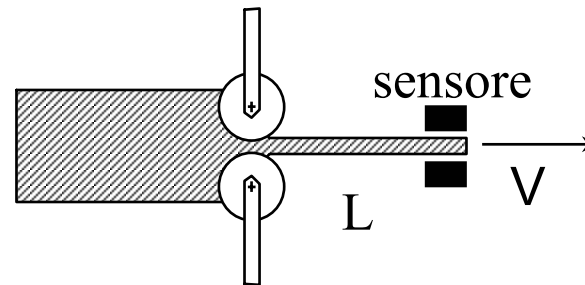
$M = 20\text{Kg}$	$\omega_r = 50$
$m = 5\text{Kg}$	$K = 50^2 \cdot m$



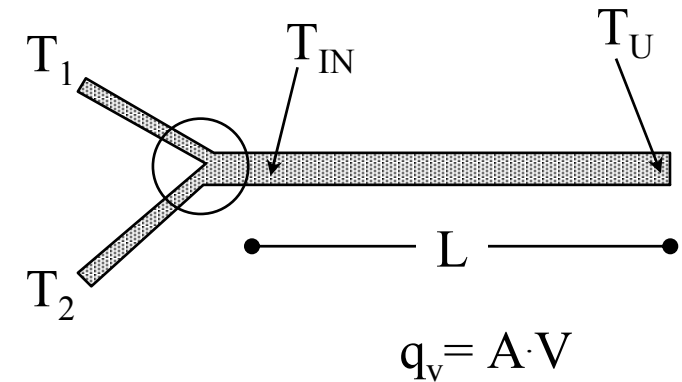
SISTEMI CON RITARDO FINITO (VEDI MARRO PAR.4.7)



$$q_u(t) = q_i\left(t - \frac{L}{V}\right)$$



$$d_{\text{mis}}(t) = d\left(t - \frac{L}{V}\right)$$



$$T_U(t) = T_{\text{IN}}\left(t - \frac{L \cdot A}{q_V}\right)$$

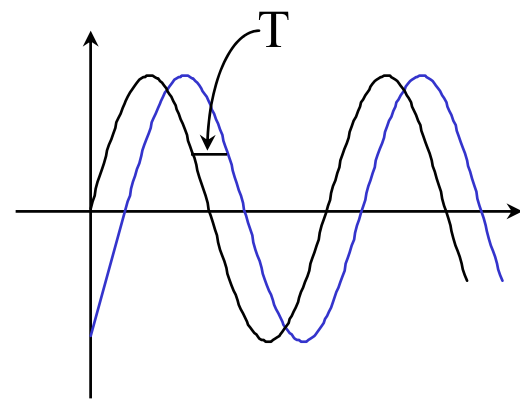
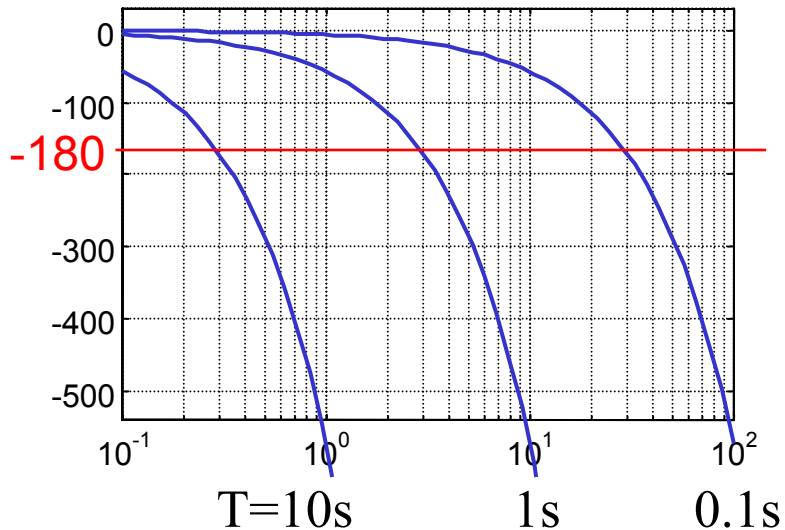
SISTEMI CON RITARDO FINITO

• Teorema della traslazione nel tempo $L[f(t - T)] = e^{-sT} L[f(t)]$ con $T = \text{cost.}$

• Possibili approssimazioni :

$$\begin{cases} e^{-sT} = 1 - sT + \frac{s^2 T^2}{2} - \frac{s^3 T^3}{3} + \dots & \text{(Taylor)} \\ e^{-sT} = \frac{1 - \frac{sT}{2}}{1 + \frac{sT}{2}} & \text{(Padè)} \end{cases}$$

• Risposta in frequenza $u(t) = \sin(\omega t)$ $y(t) = \sin\left[\omega t - \overbrace{\omega T}^{\varphi}\right]$

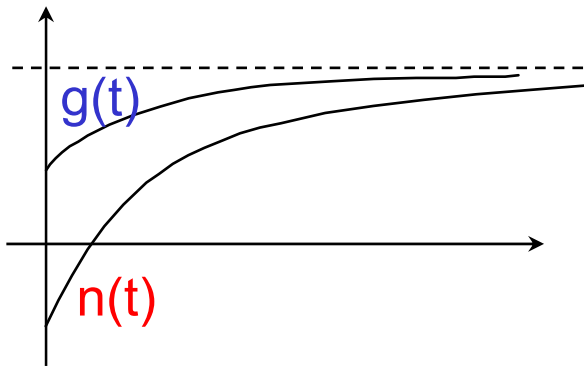


SISTEMI A FASE NON MINIMA

Hanno **zeri a parte reale positiva**: $G(s) = \frac{1 + as}{1 + bs}$ $N(s) = \frac{1 - as}{1 + bs}$

$t = 0$ $\lim_{s \rightarrow \infty} s \cdot \frac{1 \pm as}{1 + bs} \cdot \frac{1}{s} = \pm \frac{a}{b}$
 $t = \infty$ $\lim_{s \rightarrow 0} s \cdot \frac{1 \pm as}{1 + bs} \cdot \frac{1}{s} = 1$

Risposta a gradino



Ad uno **stimolo positivo** rispondono inizialmente con uno **spostamento negativo**.
Confondono il meccanismo della controreazione!

